一般的波动程论 波函数 基本概念 具体例子

 $\psi(x,t) = \vec{A}e^{i(kx-wt)} = \vec{A}e^{i\phi}$

相接 = $\frac{1278}{0110}$ $\vec{V} = \frac{w}{|k|}\hat{k}$ $v = (\frac{\partial x}{\partial t})_v = \frac{-(\partial y/\partial t)_x}{(\partial y/\partial x)_t} = \frac{w}{k}$

 $\psi(x,t) = \overrightarrow{A} \frac{1}{(x-ut)^2+1}$

5 D24 = 1/2 324

 $\psi(x,y,t) = \vec{A}e^{i(kx+k_yy-wt)}$

百谐波(20) $v = \sqrt{\frac{w}{k^2 + k_i}}$

脉冲波(10)

球面波(30)

V=U

简谐波(10)

一种(广义)的物胜场的时经分布

 $\psi(x,y,z,t) = \psi(r,\theta,\phi,t) = \frac{\bar{A}}{r}e^{i(br-wt)}$ 就量身恆 PEV = PE 4TT Sr = Const PE & / YIXITI 14x,t)1 x ==

TY = 13 (12 34) = 34 + 234 = 13 (14)

 $\Rightarrow \frac{1}{r} \frac{\partial^2}{\partial r^2} (r\psi) = \frac{1}{r^2} \frac{\partial^2 \psi}{\partial r^2} \Rightarrow \frac{\partial^2}{\partial r^2} (r\psi) = \frac{1}{r^2} \frac{\partial^2}{\partial r^2} (r\psi)$ $\Rightarrow r\psi(\vec{r},t) = Ae^{i(\vec{k}\cdot\vec{r}-wt)} \Rightarrow \psi(\vec{r},t) = \frac{A}{r}e^{i(\vec{k}\cdot\vec{r}-wt)}$

波动方程

一指导 O寻找对偶场 A us. B ②建立建合关系 24在 = 以及臣 24度 = 月之在 时间偏差 医间偏差 四解耦合 $\frac{\partial_{x}^{2}\psi(x,t)}{\partial_{x}^{2}\psi(x,t)} = v^{2}\partial_{x}^{2}\psi(x,t) + \int_{0}^{\infty} \int_{$ 四波派 花解 (MID高谐波为例) 通解 | 将解 考数拟的 10高谐波 特例 城面

相面

 $\partial_t^2 \vec{A} = d \partial_x \partial_z \vec{B} = \alpha \beta \partial_z^2 \vec{A}$

 $\partial_t^2 (\psi(x,t)) = v^2 \partial_x^2 (\psi(x,t))$

 $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$

 $\psi(x,t) = \vec{A}e^{i(kx-wt)}$

 $\psi(x,t) = f(x+vt) + g(x-vt)$

波动方程的形式决定了波函数的形式 被动方程的考数决定了被函数的考数

 $\nabla^2 = \frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial}{\partial r}) + \frac{1}{r^2} \frac{\partial}{\partial \theta^2} + \frac{d^2}{\partial \theta^2}$

Ulrito ≈ Aei(Eir-wt)

 $\frac{\partial^2 \psi}{\partial x^2} = \frac{1}{v^2} \frac{\partial^2 \psi}{\partial t^2} \Rightarrow \psi(x,t) = \tilde{A}e^{i(kx - wt)}$

 $\frac{1}{r}\frac{d}{dr}\left[r\frac{d\varphi(r)}{dr}\right] - \chi\varphi(r) = 0$ Bessel 33

 $\nabla^{2} = \frac{1}{r^{2}} \frac{\partial}{\partial r} \left(r^{2} \frac{\partial}{\partial r} \right) + \frac{1}{r^{2} \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial}{\partial \theta} \right) + \frac{1}{r^{2} \sin \theta} \frac{\partial^{2}}{\partial \theta^{2}}$

 $\frac{\partial^2}{\partial v^2}(r\psi) = \frac{1}{v^2} \frac{\partial^2}{\partial v}(r\psi) \implies \psi(r,t) = \frac{\vec{A}}{r} e^{i(\vec{k}\vec{r} - wt)}$

 $\frac{1}{r}\frac{\partial}{\partial r}(r\frac{\partial \psi}{\partial r}) = \frac{1}{V^2}\frac{\partial^2 \psi}{\partial t^2} \qquad \psi(r,t) = \varphi(r)T(t)$

电磁波

 $\begin{cases}
M1 & \vec{\nabla} \cdot \vec{E} = \frac{P}{E} \\
M2 & \vec{\nabla} \cdot \vec{B} = 0
\end{cases}$

Maxwell's Equation

Electric - Magnetic Equation $\Rightarrow \begin{cases}
\partial_t^2 \vec{E} = \frac{1}{EM} \nabla^2 \vec{B} \\
\partial_b^2 \vec{B} = \frac{1}{EM} \nabla^2 \vec{B}
\end{cases}$

 $M2 \quad \vec{\nabla} \cdot \vec{B} = 0$ $M3 \quad \vec{\nabla} \times \vec{E} = -\frac{2\vec{B}}{2t}$ $M4 \quad \vec{\nabla} \times \vec{B} = \mu(\vec{J} + z \frac{2\vec{E}}{2t})$

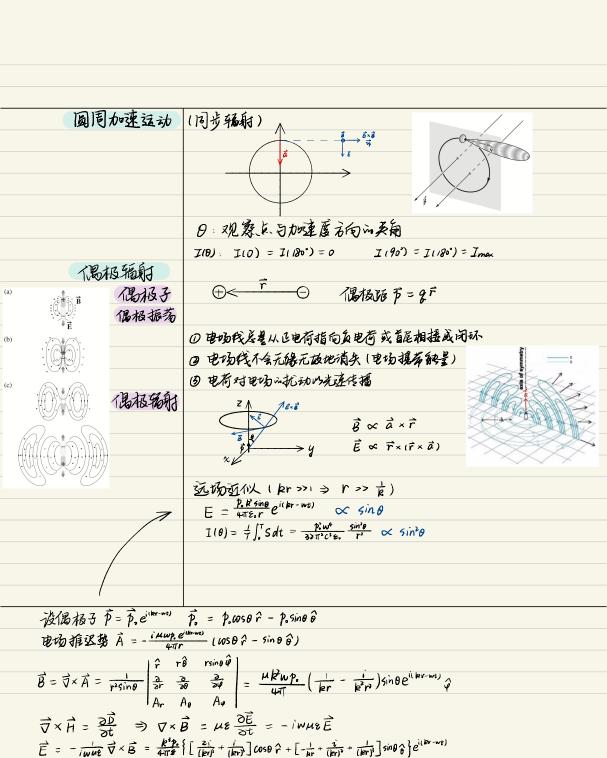
电场 VS 磁场

波动方程

对偶场

光的性质 辐射 光星是公司生的 加建运动的电荷辐射电路波 辐射 波动方程m被源板 & CE = C'PE + Source 数学描述 波动方程 | Maxwell's Equation $\{ \vec{\neg} \cdot \vec{E} = \vec{\xi} \quad \vec{\neg} \cdot \vec{B} = 0 \}$ $\{ \vec{\neg} \times \vec{E} = -\lambda_{\vec{E}} \vec{B} \quad \vec{\neg} \times \vec{B} = M(\vec{J} + \epsilon \lambda_{\vec{E}}) \}$ マ×(マ×毛) = マ(マ·毛) - マモ = デロアーマ音 $= -\partial_t (\vec{\nabla} \times \vec{B}) = -\mu \partial_t \vec{J} - \mu \epsilon \partial_t^2 \vec{E}$ $\Rightarrow \partial_t^2 \vec{E} = c^2 \nabla^2 \vec{E} - \frac{1}{\epsilon} (\partial_t \vec{J} + c^2 \nabla \rho)$ 电流速度 j=net j=net + O 系统 0 加速运动的点电荷 SP(F,t) = S(F-F(t)) $\vec{J}(\vec{r},t) = \rho q \vec{v} = q \vec{v}(t) \delta(\vec{r} - r(t))$ ② 异线中的加速电流 何子(郑福振、张照度) a ① 电荷对电场的抗动的光速传播 匀加速运动点电荷 S () 以外的 I E 應審到的基本財訓節的电场 ○ M内心工匠葵盖到 的是t, 时刻后的电场 回电场线是连续的 **连接IE和IE对应的地的践得到IE** $\vec{E} \times \vec{B}$ $\vec{B} \propto \vec{a} \times \vec{r}$ Ex Fx(Fxa) 拓照度 I(0) = I(180') = 0 I(90') = I(270') = Imax

 $\vec{E} \times \vec{B}$



色数 概念

不同颜色的光在介质中发生分散 不同频率的光在介质中折射率不同

 \bigcirc M3 $\overrightarrow{\nabla} \times \overrightarrow{E} = -\frac{\partial \overrightarrow{B}}{\partial x}$ $\vec{\Theta} \quad MI \qquad \vec{\nabla} \cdot \vec{E} = \frac{P}{\epsilon}$

四座空锋 产=磁帘 ⑤治仑数力 f=pE+j×B

WY \$\vec{\beta}{\beta} \vec{\beta}{\beta} \vec{\beta}{\beta} \vec{\beta}{\beta} \vec{\beta}{\beta} \vec{\beta}{\beta} \vec{\beta}{\beta} \vec{\beta}{\beta}

(单个电偶极子) 电偶极振荡函数

 $\vec{\nabla} \times \vec{B} = \mathcal{M}(\vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t})$

波动话程

耦合场

波动方程

P= Ngr

被观世界

研究对象 交

宏观世界

② 建立方程(BE动) Medix = - Mewix + g Ex WSWt

0 M4

通服 x(t) = a wswst + d'sinwst + pwswt + p'sinwt

特解 { 市办始条件 x(t=0) 的位移和速度在物理上不重要 x = x'=0

| 驱动同相位 p'=0

 $\Rightarrow \chi(t) = \frac{g_e/m_e}{w^2 - w^2} E_0 \omega s w t$

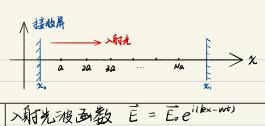
电介质

色散秦自于折射率 N = n(w)

On= C= JEH ~ NE

⑤ 介电材料中电偶极子贡献 Edgnu → ε $\vec{D} = \mathcal{E}\vec{E} + \vec{P} = \mathcal{E}\vec{E} \implies \mathcal{E} = \mathcal{E}_{+} + \frac{P}{E}$

光在介质中的传播:预射《干涉 敖射与干涉的竞争与合作 基本物程过程 全作 先单偶极子韵射再集体干涉 谁起码作用《介质各度》时, 韵射码 判据の 「历经度大时,干涉到 单个偶极子的"晏激辐射" 散射 过程 偶极子激发+偶极子辐射 (W; = W** = W。) 散射 丽频率依据 判据回 偶极激发 u=BE 入射光心或靠近如, 激发或大 福姆 I = 中心 sin'o 入射光必越大,辐射越强 何子 端利散射 稀薄外层大气⇒判据①⇒散射码 Wint < Wint > 判据② > 蓝光更散射 敬射体R度小 d~元 干涉 多个偶极子的辐射波之间的干涉 过程 判据图 入射光方向决定相击/相消于涉后向 相去干涉 顺着入射光和 人名在低中总量向新传播 相消干涉 溢着,侧向 《尽籍时向后额射、但向后的数射干涉相消》 极学证明 一维系统中心光向前相长,向后相消 12F63



干涉证相长相消活向 系统

散射体(偶极子)位置 Xn = na

动力学过程

光传播 入射光激发偈极振荡》偶极辐射出次级波》各次级波在接收屏止于涉

①偶极振荡 Un 著n个偶极引偏急平衡位置的位移 节 = Q CC

②隐极辐射 层(x,t) 著水作品极子发射的电磁波

被动方程 是 = ~ v·及 = + 方 = v·及 = + 2 克 S(x-na)

Ēn(X,t)的展 Ēn(X,t) ~ Ēn(X,t) + Ēn(X,t) (通解f(X+VE)+g(X-VE)) $E_n^{t}(x,t) \propto e^{i[tk|x-na)-wt+kna+1]}$

ロ まんなな行油

(x-na)~从活源(x=na)发出的波的相位积累 /

②继承自源点处倡极振荡 Un in 自莽相位 └ ③ Ün相对于 Ün in相位延迟 Ün ∝ -eilkna-we) = eilk

前屏上的干涉(x=x):右行被的相加

 $E_{\vec{n}}(x,t) = \sum_{n=1}^{\infty} E_{n}^{\dagger}(x_{n},t) = \sum_{n=1}^{\infty} E_{n}e^{i[k(x_{n}-na)-wt+kna+\pi]} = E_{n}\sum_{n=1}^{\infty} e^{i(kx_{n}-wt+\pi)} = n E_{n}e^{i(kx_{n}-wt+\pi)}$

⇒ n个子按约同相,相长干涉

后屏上m于涉(x=x0):左行波的极加

 $E_{\overline{K}}\left(X_{s},t\right)=\overline{X}E_{n}\left(X_{s},t\right)=\overline{X}E_{s}e^{i\left[-kx_{s}-na\right]-wt+\ln a+\pi\right]}=E_{s}e^{i\left[-kx_{s}-wt+\pi\right]}\underline{Z}e^{i2kna}$

⇒ n个子波,相邻者相位相差 2kna

敬射红偏 入射先 教制心基本物的过程 \rightarrow z过程口 入射光澈发散射子(电偶子) 冰振荡 ⇒ 偏极激发 讨程回 电偶子激发后会向四周发射次级波 > 偶极辐射 车级射光的电场方向 入射光 辐射光砖 > ₹ 电偶相子 辐射光强 1 4 光的强度 光的传播和 散射光传播方向 入射光偏振方向 欠方向 出方向 と方向 有敬射 散射克 酶射 无额射 y - 宿振 偏振的治疗的 竹扁框 有級射 有秘射 无散射 X-偏振 X偏振 ×偏振 有极射 有級射 有额射 够光 偏抵有X、好的 (有×、y-扁根) 好局板 ×偏振 4-残俗光 x-残偏光 自然光

入射面为水平平面(於=0) 劣的传播 折射和反射 物程系统 尼知: 入射光而被函数 $\vec{E}_i = \vec{E}_i^i e^{i(\vec{k}_i \vec{r} - w_i t)} = (\vec{E}_i^{\alpha}, \vec{E}_i^{\alpha}) e^{i(\vec{k}_i x + \vec{k}_i z - w_i t)}$ 参数 5 >新光 (Ei, ki, wi)=(Ei, Ei, Ei, ki, ki=0, ki, wi) 总参数 6 国由参数 4 $(\vec{E_r}, \vec{k_r}, w_r), (\vec{E_t}, \vec{k_t}, w_t)$ 差数 7 自略数 5 (不预设 於=0, 能=0)

张着松

考数的代化

月龄数

的选取

入射光

引入入射光和反射光的 쭲动二维生林系,该生林系垂直于相应的波头,

由生标轴(s. P.m.)张成 S: Senkrecht (垂真) p: parallel (孝行)

 $\hat{p} \times \hat{s} = \hat{k}$

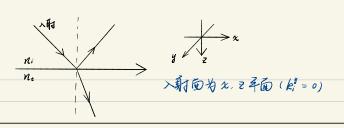
(Wi, Bi, Ei, Ei)

 $\Rightarrow (w_i, k_i^x = \frac{w_i n_i}{c} \sin \theta_i, k_i^z = \frac{w_i n_i}{c} \cos \theta_i, E_i^w = E_i^p \cos \theta_i, E_i^{a_i}, E_i^{a_i} = -E_i^p \sin \theta_i)$ I Wr. Or, Ery, Er, Kr)

反射光 $\Rightarrow (W_r, R_r^x = \frac{w_r n_r}{C} \sin \theta_r, R_r^y = 0, R_r^z = -\frac{W_r n_r}{C} \cos \theta_r, E_r^{ox} = -E_r^P \cos \theta_r, E_r^{oz} = -E_r^P \sin \theta_r)$

折射光 (Wt, Ot, Et, Et, Et)

 $\Rightarrow (W_t, k_t^x = \frac{W_t n_t}{C} \sin \theta_t, k_t^y = 0, k_t^z = \frac{W_t n_t}{C} \cos \theta_t, E_t^{ex} = E_t^P \cos \theta_t, E_t^{ey}, E_t^{ex} = -E_t^P \sin \theta_t)$



波动方程

波函数

耦合关系 Maxwell 方程 2. E = V(2) VE + 边界条件

解耦合 光源 入射光

对偶场

预解式

代入波动方程

<u>3</u>)

波动方程 ZiĒ= Viz)√Ē+Ē; Θ(-z)

电场切向连续

Mi = Me = 1

1) 当至70時 発色= なで ا (د

 $\begin{cases}
\vec{E}_{x-y}(z=\sigma) = \vec{E}_{x-y}(z=\sigma) \\
\vec{B}_{x-y}(z=\sigma') = \vec{B}_{x-y}(z=\sigma')
\end{cases}$

 $\vec{E} = (\vec{E_i} + \vec{E_r}) \cdot \theta(-\vec{z}) + \vec{E_t} \cdot \theta(\vec{z})$

验证解的形式 求解解的参数

2<0 预解式成立,且带=后

 $\overrightarrow{B}_{x-y}(z=o^-) = \overrightarrow{B}_{x-y}(z=o^+) \Rightarrow \overrightarrow{B}_{x}^{x-y}(z=o) + \overrightarrow{B}_{r}^{x-y}(z=o) = \overrightarrow{B}_{z}^{x-y}(z=o)$

(W; = Wr = Wt 月频 同色

 $k_i^y = k_r^y = k_t^z = 0$ 英国 $k_i^x = k_r^x = k_r^x$ 被关匹赋条件 $E_i^x + E_i^x = E_t^x$, $E_i^y + E_r^y = E_t^y$

 $\mathcal{B}_{i}^{\times} + \mathcal{B}_{r}^{\times} = \mathcal{B}_{t}^{\times}$, $\mathcal{B}_{i}^{y} + \mathcal{B}_{r}^{y} = \mathcal{B}_{t}^{y}$

物程性质(初、强震) 波的传播方向 Snell's Law 等波头面法 全反射 | 当1kilsin0; > 1kil > sin0; > kil = n; 时发经反射 等波面法表示 $\vec{E}_t = \vec{E}_t^0 e^{i(k_t^X \times + k_t^0 y - w_t t)}$ 解析表示

 $W_i = W_r = W_t$ $k_i^* = k_r^* = k_t^* = 0$ $k_i^* = k_r^* = k_t^*$ $\left\{ \begin{array}{l} W_{i} = W_{r} = W_{t} \Rightarrow \frac{|\mathbf{k}_{i}|}{n_{i}} = \frac{|\mathbf{k}_{r}|}{N_{r}} = \frac{|\mathbf{k}_{t}|}{n_{t}} \\ k_{i}^{\times} = k_{r}^{\times} = k_{t}^{\times} \Rightarrow |\mathbf{k}_{i}| \sin \theta_{i} = |\mathbf{k}_{r}| \sin \theta_{r} = |\mathbf{k}_{t}| \sin \theta_{t} \end{array} \right.$ ⇒ { Nisina; = nrsinar ⇒ Oi = On L打射) Ni Sin O: = Nt sin Ot > Snell's Law L反射)

 $|k_i| = |k_r| = \frac{w_i n_i}{c}$ $|k_t| = \frac{w_t n_t}{C}$

 $\begin{cases} k_{t}^{\times} = k_{i}^{\times} \\ (k_{t}^{\times})^{2} + (k_{t}^{2})^{2} = \frac{w_{t}^{2} n_{t}^{2}}{c^{2}} \end{cases} \Rightarrow k_{t}^{2} = \sqrt{\frac{w_{t}^{2} n_{t}^{2}}{c^{2}} - (k_{i}^{\times})^{2}}$

当 ki > /ki/= went 时, ki 为虚数 波函数变为 Et = Ei ei (kix-we) e N(ki)- 等2 沿 2 % 2 6 向 e 指数衰减

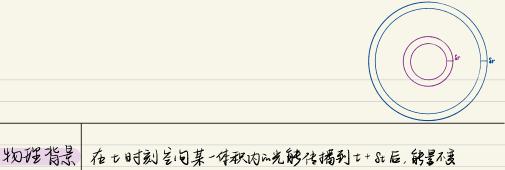
△全区射并非没有折射,而是折射光的强度沿区轴指数衰减

光纤 批打机

光行1中的光向光行2中泄漏

复阻心全国射

光心発度 Fresnell's Law 菲涅尔多律 原则 利用电场和磁场的边界条件 車場 { n×(戸,-戸)=0 (前・(京,-戸)=0 (前・(京,-戸)=0 (前・(京,-戸)=K) 特殊情形口 714 mode $\vec{B} = (0, B_y, 0) \vec{E} = |\vec{E}| \hat{p}$ 边界条件: $\begin{cases} E_i^x + E_r^x = \bar{E}_t^x \Rightarrow |E_i|\cos\theta_i - |E_r|\cos\theta_r = |E_t|\cos\theta_t \\ B_i^y + B_r^y = B_t^y \Rightarrow |B_i| + |B_r| = |B_t| \end{cases}$ $- |E-B + |B| = \frac{|E|}{v_i} = \frac{|E|n_i}{c} |B| = \frac{|E|n_i}{c} |B| = \frac{|E|n_i}{c}$ Snell 支俸 $n_i \sin \theta_i = n_t \sin \theta_t$ $\theta_i = \theta_t$ $\frac{|E_r|}{|E_i|} = \frac{n_t \omega s \theta_i - n_i \omega s \theta_t}{n_t \omega s \theta_i + n_i \omega s \theta_t} \qquad \frac{|E_t|}{|E_i|} = \frac{2n_i \omega s \theta_i}{n_t \omega s \theta_i + n_i \omega s \theta_t}$ TE made $\vec{E} = (0, E_1, 0)$ $\vec{B} = |B| \cdot (-\hat{p})$ 特殊情形② 立界文件 $\xi E_{r}^{3} + E_{r}^{3} = E_{t}^{3} \Rightarrow |E_{r}| + |E_{r}| = |E_{t}|$ (M21) $|B_{r}^{x} + B_{r}^{x} = B_{t}^{x} \Rightarrow -|B_{r}| \cos \theta_{r} + |B_{r}| \cos \theta_{r} = -|B_{t}| \cos \theta_{t}$ $E-B \not= R$ $|B_i| = \frac{|E_i|}{v_i} = \frac{|E_i|n_i}{c}$ $|B_f| = \frac{|E_f|n_i}{c}$ $|B_{f}| = \frac{|E_f|n_f}{c}$ Snell 養俸 n; sin 0; = nt sin 0t $\theta_i = \theta_t$ $\frac{|E_t|}{|E_t|} = \frac{n_t \omega_5 \theta_t - n_t \omega_5 \theta_t}{n_t \omega_5 \theta_t + n_t \omega_5 \theta_b} \qquad \frac{|E_t|}{|E_t|} = \frac{2n_t \omega_5 \theta_t}{n_t \omega_5 \theta_t + n_t \omega_5 \theta_b}$ $\rho = \frac{n_t}{n_i}$ 小猫 TM (产分量) TE (S分号) 振幅反射率 光疏→光茶 振幅透射率 光系 → 光疏



t时刻的体积 t+St时刻在折射光

(6.20)

新量身恆 物程系统

 $P_{\Gamma} = S_{1}|E_{\Gamma}|^{2} = \frac{N_{1}^{2}}{C^{2}}|E_{\Gamma}|^{2} = \frac{N_{1}^{2}}{C^{2}}r^{2}|E_{1}|^{2}$ Pe = SelEul = No 1/Eil = No 1/Eil ③强加 Uit) = Uxt+St) + Utit+St) $U_r(t+\delta t) = P_r V_r(t+\delta t) = \frac{m!}{C^2} r^2 |E_i|^2 \cdot Sh_r \omega s \theta_r = \frac{n!h!}{C^2} S|E_i|^2 \cdot r^2 n_i \omega s \theta_i = I_r \omega s \theta_i$ Utit+8t) = Pt /4+8t) = nt t/E/2 Sht WSOt = nt SIE/2 + 2nt WSOt = It was $I_i \omega s \theta_i = I_r \omega s \theta_r + I_t \omega s \theta_t$ 猪度反射率 R = 芸 = ri 锅度蓬射车 丁= ÷ = n; t2 $\begin{array}{ccc} \mathbf{p} \, \widehat{\gamma} \, \overline{\sharp} & \mathbf{s} \, \widehat{\gamma} \, \overline{\sharp} \\ \\ \widetilde{r}_{\mathsf{p}} = \widetilde{E}'_{\mathsf{lp}} / \widetilde{E}_{\mathsf{lp}} & (6.13) & \widetilde{r}_{\mathsf{s}} = \widetilde{E}'_{\mathsf{ls}} / \widetilde{E}_{\mathsf{ls}} & (6.14) \end{array}$

强度反射率 $R_p = \frac{I_{1p}'}{I_{1p}} = |\stackrel{\sim}{r_p}|^2$ (6.15) $R_s = \frac{I_{1s}'}{I_{1s}} = |\stackrel{\sim}{r_s}|^2$ (6.16) 能流反射率 $\mathcal{M}_p = \frac{W_{1p}'}{W_{1p}} = R_p$ (6.17) $\mathcal{M}_s = \frac{W_{1s}'}{W_{1s}} = R_s$ (6.18)

强度透射率 $T_p = \frac{I_{2p}}{I_{1p}} = \frac{n_2}{n_1} |\tilde{t}_p|^2$ (6.21) $T_s = \frac{I_{2s}}{I_{1s}} = \frac{n_2}{n_1} |\tilde{t}_s|^2$ (6.22)

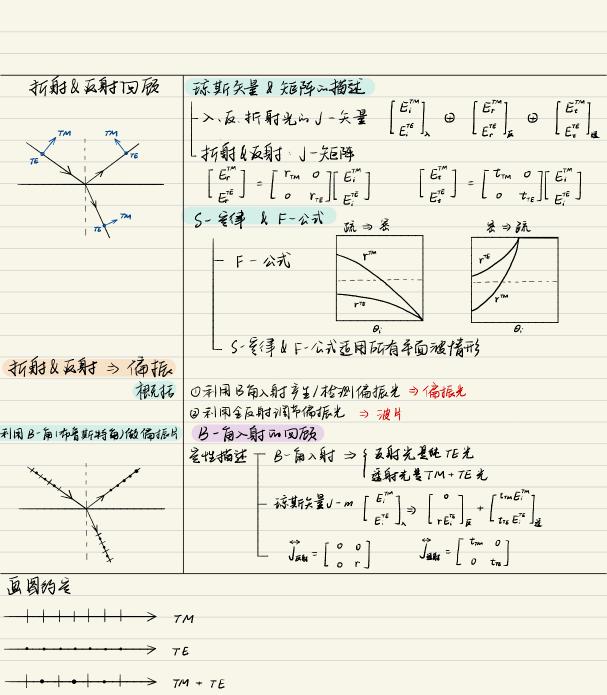
能流送射率 $\mathcal{F}_{p} = \frac{W_{2p}}{W_{1p}} = \frac{\cos i_{2}}{\cos i_{1}} T_{p}$ (6.23) $\mathcal{F}_{s} = \frac{W_{2s}}{W_{1s}} = \frac{\cos i_{2}}{\cos i_{1}} T_{s}$ (6.24)

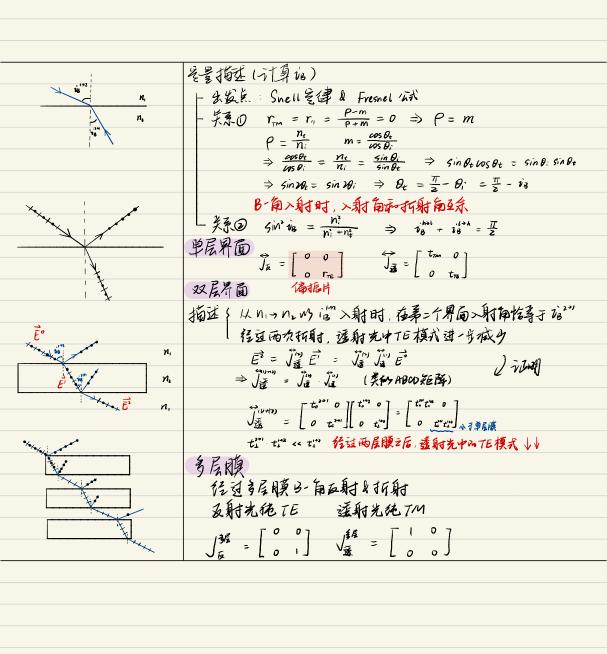
 $\widetilde{t}_{p} = \widetilde{E}_{2p} / \widetilde{E}_{1p}$ (6.19) $\widetilde{t}_{s} = \widetilde{E}_{2s} / \widetilde{E}_{1s}$

の成Vit)和Vit+St) 求解 $\left\{ \begin{array}{c} \frac{h_i}{v_i} = \frac{h_r}{v_k} = \frac{h_t}{v_k} \\ v = \frac{c}{n} \end{array} \right.$ Vitt) = Sihi = Shiwso: $V_r(t+\delta t) = S_r h_r = Shr \omega s \theta_r$ V+(t+St) = Stht = Sht WS Bt => nihi = nihr = nth, ②抗电磁场解鉴差虚 $\rho_{i} = \frac{\mathcal{E}_{i}|\mathcal{E}_{i}|^{2}}{2} + \frac{|\mathcal{B}_{i}|^{2}}{2} = \mathcal{E}_{i}|\mathcal{E}_{i}|^{2} = \frac{n_{i}^{2}}{n_{i}^{2}}|\mathcal{E}_{i}|^{2}$ $U_i(t) = \rho_i V_i(t) = \frac{n_i^2}{G^2} |E_i|^2 \cdot Shi \omega s \theta_i = \frac{n_i h_i}{G^2} S |E_i|^2 \cdot n_i \omega s \theta_i = I_i \omega s \theta_i$

振幅反射率

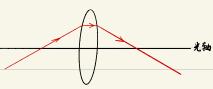
振幅透射率





以後
$$\int_{\overline{G}} = \begin{bmatrix} \sigma_{1} \\ \sigma_{2} \end{bmatrix}$$
 $\int_{\overline{G}} = \begin{bmatrix} \sigma_{1} \\ \sigma_{2} \end{bmatrix}$ $\int_{\overline{G}} = \begin{bmatrix} \sigma_{1} \\ \sigma_{2}$

独片 一功能 对两个互相垂直心局振方向,诱导不同的相任延迟 Ja=eib[0eios] - 特征指标: 协轴 对于TM. TE模式的光,相位积累(光程)少的细型快轴 考虑一个彼出,彼片中 V16 > Vm => kre < km (1= 1) 光程 PTE = RTE d < kmd = OTH Cg.若快動为TEgio, 2) めアルコタTE OダニタTE-Prin < 0 $\vec{J} = e^{i\phi} \begin{bmatrix} 1 & 0 \\ 0 & e^{i(\phi_{10} - \phi_{10})} \end{bmatrix} = e^{i\phi} \begin{bmatrix} 1 & 0 \\ 0 & e^{i\alpha\phi} \end{bmatrix}$ _ example 入射光 袁波片~ 0户= 翌=五 拉独的~ 20= 笠= 芸 我偏[:] 椭偏[zei](~~~) 桶偏 [20] (報 我偏 [[]~[] 椭偏 [ex] 圆庙[!] 相偏 椭偏 椭偏 自然 自然 自然



物程系统 光 光沿直线传播 Snell's Law $\{\theta_i = \theta_r \mid n_i \sin \theta_i = n_t \sin \theta_t \}$ 光学元太件 存在一个对称轴 > 光轴 光轴 0 ≈ 0° 数学建模 用最简单的一中数字完整地描述光线 光学元器件 原则 光等无条件的作用是把一本入新光度成一束外打充 数字模型 $\begin{cases} h_4 = f_1(h_1, \theta_n) \end{cases}$ 数字模型 $\begin{cases} h_4 = f_1(h_1, \theta_n) \end{cases}$ 数据数 $\begin{cases} h_4 = ah_1 + b\theta_n \end{cases}$ $\begin{cases} h_4 = ah_1 + b\theta_n \end{cases}$ $\begin{cases} h_4 = ah_1 + b\theta_n \end{cases}$ ABCID矩阵 光学元器件由 (a, b, c, d) 4个数字确定 $\begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} h_{2} \\ \theta_{4} \\ \chi \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} h_{2} \\ \theta_{3} \\ \chi_{3} \end{bmatrix}$ 停轴近似 线性近似(f., f.)

光望元恭件年19
単介光望元恭件
東海 中 大 + (スース)
$$4\pi$$
 の 4π の π の π

$$\frac{1}{1} \left[\begin{array}{c|c}
 & x_n \\
 & x_n \\$$

薄凸透镜

Max =
$$\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}_{R}$$
 $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}_{R}$ $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}_{R}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) & \frac{n_{k}}{n_{k}} \end{bmatrix}$ = $\begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n}{n_{k}}-1) &$

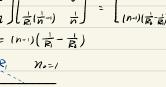
$$= \begin{bmatrix} \frac{1}{R} \left(\frac{N_n}{N_n} - 1 \right) & \frac{N_n}{N_n} \end{bmatrix}$$

$$= \begin{bmatrix} \frac{1}{R_n} \left(n - 1 \right) & n \end{bmatrix}$$
電腦 $\frac{1}{L} = 1$

$$= \begin{bmatrix} 1 & 0 \\ \frac{1}{R}(n-1) & n \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{1}{N}-1) & \frac{1}{N} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ (n-1)(\frac{1}{R}-\frac{1}{R}) & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix}$$

$$\text{Re } f \qquad \frac{1}{f} = (n-1)(\frac{1}{R}-\frac{1}{R})$$

$$\text{Re } N_{\bullet=1}$$





焦距于 = (n-1)(点+点)



$$\left| \left(\frac{1}{R} \left(\frac{1}{R} - 1 \right) - \frac{1}{R} \right) \right|^{2} = \left| \left(R - 1 \right) \left(\frac{1}{R} - \frac{1}{R} \right) \right|$$

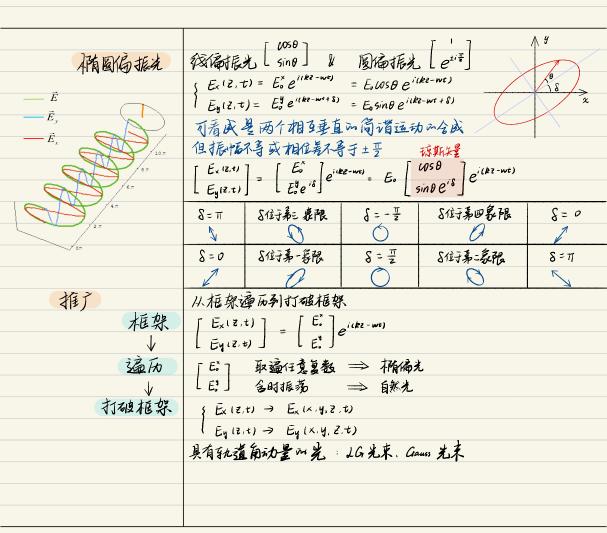
$$\left| \left(R - 1 \right) \left(\frac{1}{R} - \frac{1}{R} \right) \right|$$

$$\left| \left(R - 1 \right) \left(\frac{1}{R} - \frac{1}{R} \right) \right|$$

 $\mathcal{M}_{\widehat{\mathbf{k}}\widehat{\mathbf{i}}} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R}(1 - \frac{n_{\bullet}}{n_{\bullet}}) & \frac{n_{\bullet}}{n_{\bullet}} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n_{\bullet}}{N_{\bullet}} - 1) & \frac{n_{\bullet}}{n_{\bullet}} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R}(1 - \frac{n}{n_{\bullet}}) & \frac{n_{\bullet}}{n_{\bullet}} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{R}(\frac{n_{\bullet}}{n_{\bullet}} - 1) & \frac{n_{\bullet}}{n_{\bullet}} \end{bmatrix}$

 $= \begin{bmatrix} 1 & 0 \\ \frac{1}{16}(1-n) & n \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{16}(\frac{1}{10}-1) & \frac{1}{10} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ (1-n)(\frac{1}{16}+\frac{1}{16}) & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -\frac{1}{4} & 1 \end{bmatrix}$

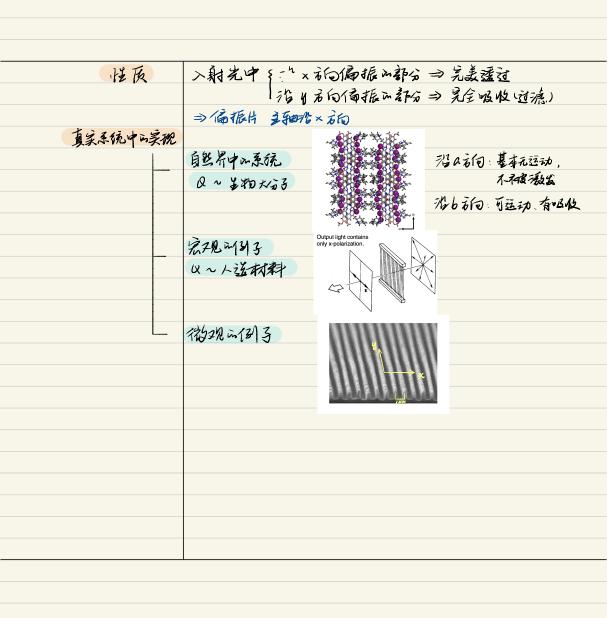
偏振 波函数 $\frac{\partial^{2}\vec{E}}{\partial x^{2}} + \frac{\partial^{2}\vec{E}}{\partial x^{2}} + \frac{\partial^{2}\vec{E}}{\partial x^{2}} = n\epsilon \frac{\partial^{2}\vec{E}}{\partial x^{2}} \\
\frac{\partial^{2}\vec{E}}{\partial x^{2}} + \frac{\partial^{2}\vec{E}}{\partial x^{2}} + \frac{\partial^{2}\vec{E}}{\partial x^{2}} = n\epsilon \frac{\partial^{2}\vec{E}}{\partial x^{2}} \\
\frac{\partial^{2}\vec{E}}{\partial x^{2}} + \frac{\partial^{2}\vec{E}}{\partial x^{2}} + \frac{\partial^{2}\vec{E}}{\partial x^{2}} = n\epsilon \frac{\partial^{2}\vec{E}}{\partial x^{2}}$ (辰,台, 后)可以取不同的独函数 自然光(无偏振光) 名的石无优级性 $\begin{cases} \dot{E}_{x} = E_{0}s\theta = E_{0}cos\theta e^{i(kz-wt)} = E_{0}^{x}e^{i(kz-wt)} \\ E_{y} = E_{0}sin\theta = E_{0}sin\theta e^{i(kz-wt)} = E_{0}^{y}e^{i(kz-wt)} \end{cases} \Rightarrow \chi$ 我偏振先 $\begin{bmatrix} E_{x}(z,t) \\ E_{y}(z,t) \end{bmatrix} = \begin{bmatrix} E_{0}^{x} \\ E_{0}^{y} \end{bmatrix} e^{i(kz-wt)} = E_{0} \begin{bmatrix} ws\theta \\ sin\theta \end{bmatrix} e^{i(kz-wt)} = E_{0}^{x} \begin{bmatrix} 1 \\ tan\theta \end{bmatrix} e^{i(kz-wt)}$ 球斯夫量 ~ { [Ex]; [wso]; [tano] } 部分偏振光 介于自然无和战偏先之间 $\begin{cases} E_{x} = E_{0} W S(kz - wt) = Re[E_{0} e^{i(kz - wt)}] \\ E_{y} = E_{0} W S(kz - wt \pm \frac{\pi}{2}) = Re[E_{0} e^{i(kz - wt \pm \frac{\pi}{2})}] \end{cases}$ 圆偏抵光 $\begin{bmatrix} E_{x}(z,t) \\ E_{y}(z,t) \end{bmatrix} = E_{z} \begin{bmatrix} 1 \\ e^{i\frac{\pi}{2}} \end{bmatrix} e^{i(kz-mt)}$ 逆时针 (左旋圆偏振光) 11级时针(右旋图编振光) $\begin{cases} \bar{E}_{x} = \bar{E}_{0} \cos(kz - wt) \\ E_{y} = E_{0} \sin(kz - wt) \end{cases}$ $\begin{cases} E_x = E_x \omega s(kz - wt) \\ E_y = -E_x sin(kz - wt) \end{cases}$ = E wsikz-wt-=) = Lous(kz-wt+ 三)



偏振心心用 产生偏振光、检测偏振光 偏振片 一作用 性质 偷振片存在一个主轴,它工作用是过滤掉入射光中电场部向 与五轴垂直心光,只透过电场的(偏振右向)和主轴平行心光. 安号描述 超川生物 系统 (实数/复数/含时随机振荡) 御掘山(下用入射光的球斯灭量[日] 编版 出射光[日] 矢陉阵描述(玩斯矢陉阵)~ [00] (新禮 主轴///轴) 马马斯运律 Ix = Ax = (A, 1050) = A2 1050 = L, 1050 野量视角 (0克=扁振动与红轴夹角) 推广、到明和入新光偏振其的各人。 主轴2和主轴, 天角星月 E(0, Ey,0) 弱斯爱律 $I_2 = I_1 \omega s^2 \theta_2 = I_0 \omega s^2 \theta_1 \omega s^2 \theta_2$

二何色姓 基本原则是在介面中的传播性质,完全由光和介质的风的相对印刷决定 极端情况 D光和介质以及没有相对作用(光不舒涵发及m运动) 光视介质为直笔 ②光和《有相至作闸,且《心族耗》》 光不能在介质中传播 二向色性:同一介质中整分3的上两个极端情况 系统 设介质正见是加下情况 名向异性 \ 治义方向元志振动,无法被激发 名向异性 \ 治义方向有很强证据耗 波动石程 二维海振波动福 见振动 $\begin{cases} \partial_t^2 U_x = \infty \cdot U_x + E_x \Rightarrow U_x = \dot{U}_x = 0 \\ \partial_t^2 U_y = k U_y + E_y - \gamma_y \dot{U}_y \end{cases}$ $\begin{cases} \partial_t^2 \vec{E}_X = C^2 \partial_z^2 \vec{E}_X \\ \partial_t^2 \vec{E}_y = V' \partial_t^2 \vec{E}_y \quad (V = V_f + iV_i) \end{cases}$

 $\begin{cases} \partial_t \text{ tx} = C \partial_z \text{ tx} \\ \partial_b \text{ Ey} = V \partial_z \text{ Ey} \end{cases}$ $\begin{cases} E_X = E^X e^{i(kz - Ckt)} \\ E_Y = E^Y e^{i(kz - V, kt)} e^{-ikilz} \end{cases}$ $|E_{y_1}|^2$



双折射 than 1 名羽解释 真乭 双射折介质 物程过程 语言描述 TE和TM模式的光发呈不同的折射现象 物理系统 光 军面被 介质 有名向异性的 (eg. 电偶极子) Example 模型特点①电偶极子,类比为弹簧振子 ②有各向异性 { x-y 年面内可振动 论 z 的不能振动 电影极子二运动方程 (mux = kux + tx 波动方程 对偶场 相合流系 0 乾鈞律 OM4 # \$ = E DE E + J OM3 FXE = - 2B (见下反)

 $\mathcal{M}_{0} \begin{bmatrix} \mathcal{E}_{0} + \mathcal{E}_{1} & 0 & 0 \\ 0 & \mathcal{E}_{0} + \mathcal{E}_{1} & 0 \\ 0 & 0 & \mathcal{E}_{0} \end{bmatrix} \xrightarrow{\mathcal{E}_{0}^{1}} \begin{bmatrix} \mathcal{E}_{0} \\ \mathcal{E}_{1} \\ \mathcal{E}_{2} \end{bmatrix} = \begin{bmatrix} \partial_{1}^{1} + \partial_{2}^{2} & -\partial_{1} \partial_{1} & -\partial_{2} \partial_{2} \\ -\partial_{2} \partial_{1} & \partial_{2}^{2} + \partial_{1}^{2} & -\partial_{1} \partial_{2} \\ -\partial_{2} \partial_{2} & -\partial_{2} \partial_{2} & \partial_{2}^{2} + \partial_{1}^{2} \end{bmatrix} \begin{bmatrix} \mathcal{E}_{0} \\ \mathcal{E}_{1} \\ \mathcal{E}_{2} \end{bmatrix}$

波动方程

$$= \mu_{0} \left(\begin{array}{c} \dot{E}_{0} \\ \dot{E}_{0} \\ \dot{E}_{0} \end{array} \right) + \left(\begin{array}{c} n_{0}q_{0} & 0 & 0 \\ 0 & n_{0}q_{0} & 0 \end{array} \right) \left[\begin{array}{c} \dot{E}_{0} \\ \dot{E}_{0} \\ \dot{E}_{0} \end{array} \right]$$

$$= \mu_{0} \left[\begin{array}{c} \mathcal{E}_{0} + \mathcal{E}_{1} & 0 & 0 \\ 0 & \mathcal{E}_{0} + \mathcal{E}_{1} & 0 \end{array} \right] \left[\begin{array}{c} \dot{E}_{0} \\ \dot{E}_{0} \\ \dot{E}_{0} \end{array} \right] \left(\begin{array}{c} \dot{E}_{0} \\ \dot{E}_{0} \end{array} \right]$$

$$= \mu_{0} \left[\begin{array}{c} \mathcal{E}_{0} + \mathcal{E}_{1} & 0 & 0 \\ 0 & \mathcal{E}_{0} + \mathcal{E}_{1} & 0 \end{array} \right] \left[\begin{array}{c} \dot{E}_{0} \\ \dot{E}_{0} \\ \dot{E}_{0} \end{array} \right] \left(\begin{array}{c} \mathcal{E}_{1} = n_{0}q_{0} \\ \dot{E}_{1} \end{array} \right)$$

ウ×(ガ×色)-Ot(ガ×B)=-Ot(カ×B)-Mをみもら コママを=-Mをは自 M3 & M4 マ×苣=-ðt B 7 x 7 x = 7 (7 E) - 2 E = 7 (2 Ex + 2 Ex + 2 Ez) - (2 + 2 + 2 + 2) E

$$\nabla \times \vec{E} = -\partial_t \vec{B} \qquad \vec{\nabla} \times \vec{\nabla} \times \vec{E} = \vec{\nabla}(\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E} = \vec{\nabla}(\partial_x E_x + \partial_y E_y + \partial_z E_z) - (\partial_x^2 + \partial_y^2 + \partial_z^2) \vec{E}$$

$$\nabla \times \vec{B} = M_x \vec{E} \cdot \vec{A} \vec{E} \qquad = \begin{bmatrix} \partial_x^2 E_x + \partial_x \partial_y E_y + \partial_x \partial_z E_z \\ \partial_x \partial_y E_x + \partial_y^2 E_y + \partial_y \partial_z E_z \end{bmatrix} - (\partial_x^2 + \partial_y^2 + \partial_z^2) \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} = \begin{bmatrix} -\partial_y^2 - \partial_y^2 - \partial_y^2$$

 $\mathcal{U}_{0} \begin{bmatrix} \mathcal{E}_{0} + \mathcal{E}_{1} & 0 & 0 \\ 0 & \mathcal{E}_{0} + \mathcal{E}_{1} & 0 \\ 0 & 0 & \mathcal{E}_{0} \end{bmatrix} \partial_{0}^{2} \begin{bmatrix} \mathcal{E}_{x} \\ \mathcal{E}_{y} \\ \mathcal{E}_{y} \end{bmatrix} = \begin{bmatrix} \partial_{1}^{2} + \partial_{2}^{2} & -\partial_{x} \partial_{y} & -\partial_{x} \partial_{z} \\ -\partial_{x} \partial_{x} & -\partial_{y} \partial_{z} & \partial_{z}^{2} + \partial_{y}^{2} \end{bmatrix} \begin{bmatrix} \mathcal{E}_{x} \\ \mathcal{E}_{y} \\ \mathcal{E}_{z} \end{bmatrix}$ $= \begin{bmatrix} \partial_{1}^{2} + \partial_{2}^{2} & -\partial_{x} \partial_{y} & -\partial_{x} \partial_{z} \\ -\partial_{x} \partial_{z} & -\partial_{y} \partial_{z} & \partial_{z}^{2} + \partial_{y}^{2} \end{bmatrix} \begin{bmatrix} \mathcal{E}_{x} \\ \mathcal{E}_{y} \\ \mathcal{E}_{z} \end{bmatrix}$

没动方程

$$\frac{2}{R_{ij}} = |R| \begin{bmatrix} \sin\theta \cos\theta \\ \sin\theta \sin\theta \end{bmatrix}$$

$$\frac{2}{\sin\theta} = |R| \begin{bmatrix} \sin\theta \sin\theta \\ \sin\theta \sin\theta \end{bmatrix}$$

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$$\frac{2}{\sin\theta} = |R| \begin{bmatrix} \sin\theta \cos\theta$$

本次核性話程組ェルル平積解 制的关系 (IEI, Ê, IRI) 依頼 (Ĝ(B, 19), w)

ス次方程整理成 $\int \begin{bmatrix} \vec{G} \\ \vec{E} \end{bmatrix} = \alpha \begin{bmatrix} \vec{G} \\ \vec{E} \end{bmatrix}$ ⇒ 式生体転失系

电场液函数
$$\vec{E} = \begin{bmatrix} E_x \\ E_y \end{bmatrix} e^{i(|\mathbf{r}|\hat{\mathbf{k}}|\hat{\mathbf{r}} - \mathbf{w}t)} = |E| \begin{bmatrix} E_y \\ E_y \end{bmatrix} e^{i(|\mathbf{r}|\hat{\mathbf{k}}|\hat{\mathbf{r}} - \mathbf{w}t)}$$

$$\mu_0 w^2 (\hat{\mathbf{r}})^{-1} \hat{\mathbf{r}} \hat{\mathbf{m}} + \hat{\mathbf{m}} \hat{\mathbf{m}$$

$$|E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}} \qquad |E_{z}| = \frac{\omega}{c} \sqrt{\frac{z(z + z)z}{2z + z_{1} - z_{1} \cos 2\theta}}$$

⇒ 介电常数 笞= | exy

双折射的性质和视象 性质

介质的姓居

传播光的性质和视象

传播和和偏振和

光心性质

回顾折射率的影

双折射晶体(正常光

反射光流打射率

1 B = F

先发点

依赖于波尔布(8)

▶ 正晶体 ↑k_z (optical axis)

传播的、海振响、传播速度、光的强度 传播酒 { 波失而 }

循振箱 E田D, FI, B 电场方向

独场面 Maxwell's Equations &

B=NH,在一般介质中以=M=1 > B=H

M1: $\vec{\nabla} \cdot \vec{D} = P = 0 \Rightarrow (i\vec{k}) \cdot \vec{D} = 0 \Rightarrow \vec{k} \cdot \vec{D} = 0 \qquad \vec{k} \perp \vec{D}$

OBF ③ 4/Maxwell旅程

推导

M2 7 B = 0 ⇒ R B = 0 M3: vxĒ=-aB ⇒ (ik)×Ē= iwB ⇒ k×Ē=wB

 $M4: \vec{\nabla} \times \vec{H} = \partial_0 \vec{D} \implies (i\vec{k}) \times \vec{H} = -i\omega \vec{D} \implies \vec{k} \times \vec{H} = -\omega \vec{D}$

光学中,介度的好历由折射参维·描述

双折射 双折射革 ○介质中存在两个折射率 n= & = C/RI × IkI nod = C/kod/ = C/MO Exy

 $N_{\text{ex}} = \frac{C}{W | \text{key}} = C \sqrt{\frac{2M_0 \, \text{Eng St}}{\text{Sug + St + (St - Sug) (COS 20)}}} \frac{0 = 0}{\text{2505 southly}} C \sqrt{M_0 \, \text{Eng}}$ 光在介质中传播,可能,应差到两种折射率,依赖于光~偏振

▶ 负晶体 ↑k_z (optical axis)

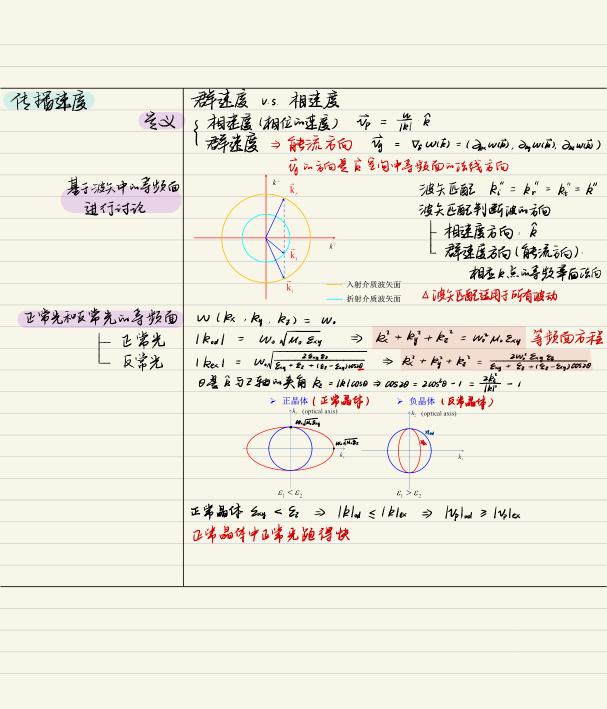
当光沿主轴(即z轴)传播时,反常光退化为正常光,即 No.(0=0)= No.(0=0)

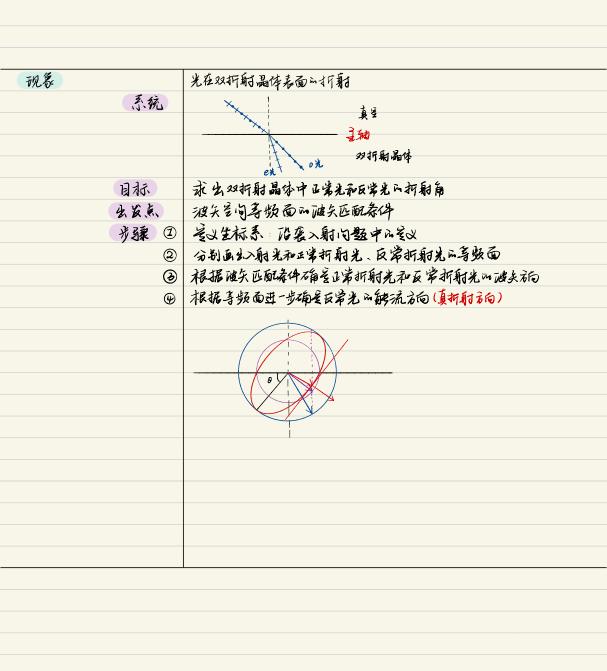
| 的流淌了《EXA(触流淌望真的传播活向) FS

孟面被解 ① Ē. D 由 D = 笔Ē ⇒ D 与 Ē不平行, 英角的 D Ē | = IEIIDIOS → D SQ = IDIEI

> BIR BIE DIR DIH

@ 香流 s= Ē×前 ⇒ SIÈ SIÀ





双折射晶体介面处的折射 折射的物程图像 系统 界面处的折射和吸射 (双扩射晶体表面》)

>射光激发界面上的 Q 酸氢激振荡 > Q 辐射次级波 >次级被相长/相指干涉 $\begin{cases} \ddot{x} = kx + E_x^{in} \\ \ddot{y} = ky + E_y^{in} \end{cases}$

原则

折射的是是描述 反常光m多频率面

波天匹配 kin = kind = kex

 $k_z = |k| \cos \theta \Rightarrow \cos 2\theta = 2\cos^2 \theta - | = \frac{2k_z^2}{|k|^2} - |$

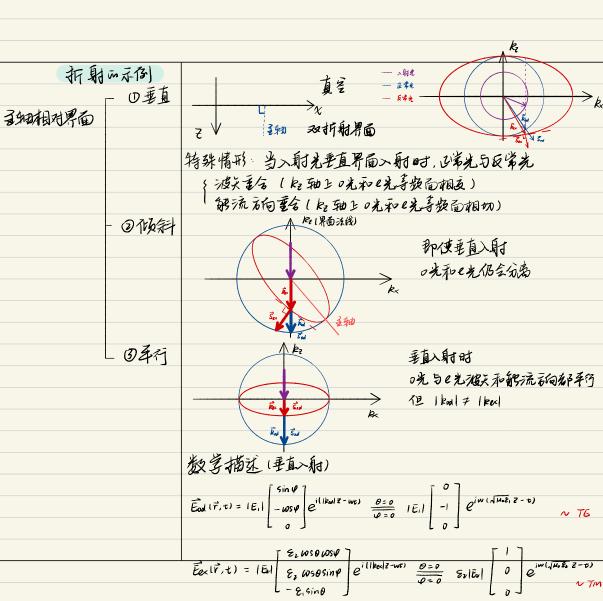
=> |k|2 [Exy + Ez + (Ez - Exy) (2k2 - 1)] = 2M, W2 Exy Ez

=> (Exy + Ez)|k|2 + (Ez - Exy)(2kz - |k|2) = 2M. W. Exy &z

=) $\frac{k_x^2 + k_y^2}{\mu_0 w_1^2 \xi_{22}} + \frac{k_z^2}{\mu_0 w_1^2 \xi_{xy}} = 1$

=> Exy (ki+ ky) + Ez ki = 1000, Exy &

 $\sigma = \arctan \frac{\mathcal{E}_{x_1} k^x}{\mathcal{E}_{x_2} k^2}$

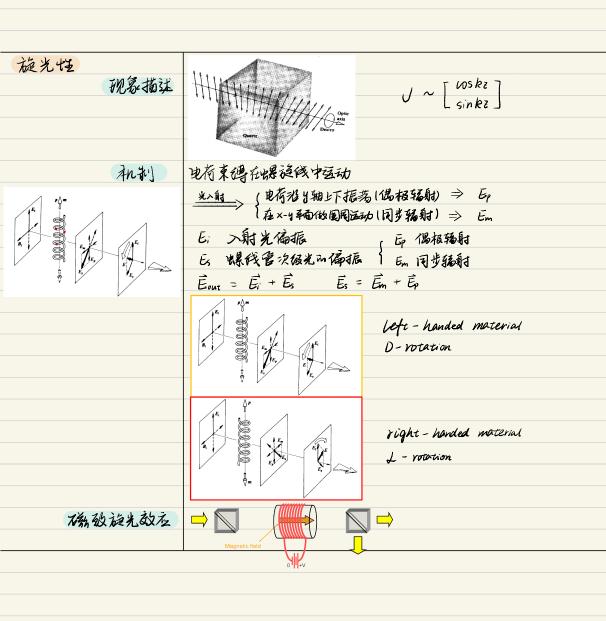


正常光和五常光传播的年行 正常光和五常光偏振的垂直 正考光和五考光 1月不同 ⇒ ハス同

⇒ 用来做油片

双折射充气器体

波片	回版	海片的球斯矩阵
		入射光 $\begin{bmatrix} E_i^x \\ \bar{E}_i^z \end{bmatrix}$ 名射光 $\begin{bmatrix} \bar{E}_o^x \\ \bar{E}_o^z \end{bmatrix} = \begin{bmatrix} e^{i\phi_a} & o \\ o & e^{i\phi_a} \end{bmatrix} \begin{bmatrix} \bar{E}_i^x \\ \bar{E}_i^z \end{bmatrix}$
		E' Lo e' JE' J
	双折射	eir. O Piar
	设置	先轴平行于界面;入射光垂直入射时,有亚还作用
		₹₩ · · · · · · · · · · · · · · · · · · ·
	系统	→ 養
		(D7-w+1 [17 illy (20)-w+20]
		$7E \qquad \begin{bmatrix} 0 \end{bmatrix} e^{i(k\bar{z}-wt)} \qquad \begin{bmatrix} 0 \end{bmatrix} e^{i[k\omega(\bar{z}-v)-wt+w]} \qquad \begin{bmatrix} 0 \end{bmatrix} e^{i[k\bar{z}-d)-wt+v_0^w]}$
		7M [] e (kz-wt) [] e [[] e [[[] e [[] e [[] e []] e [[] e
		Ψ. = O
		(φ_d^{od}) = $k_{\text{od}} d + \varphi$. = $k_{\text{od}} d$ (φ_d^{ex}) = $k_{\text{ex}} d + \varphi$. = $k_{\text{ex}} d$
		Ei = or Ete + pErm = [p]ei(kz-wt) 双打射晶体加J-矩阵
		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
		[o eies] [B]
		对垂直入射光,厚度为d in 双折射晶体(光轴平行界面) 的作用
		可由了矩阵 eing [o eing 描述,即这块品体经到了被片中作用
分束器	_	
	功的要求	Optic axis n _o = 1.66 n _b = 1.55
	李134	Vicol Prism Brewster's Angle Optic axis (out of page)
	•	Glan-Thompson and Glan-Air Polarizer
Wollaston polarizing beam splitter		
0-ray X		
↑ C B		



民结

光学加2个范式 1 介质统-由折射率 1. 描述 2 売れい意义 指导坚健障路 指导打破范式 范式的集结 Q U $\partial_{z}^{z} \begin{bmatrix} u_{x} \\ u_{y} \\ u_{z} \end{bmatrix} = -w^{z} \begin{bmatrix} u_{x} \\ u_{y} \\ u_{z} \end{bmatrix} + \frac{2}{m} \begin{bmatrix} E_{x} \\ \bar{E}_{y} \\ \bar{E}_{z} \end{bmatrix}$ 色被 $\mathcal{M}(w)$ $\partial_{t}^{2} \begin{bmatrix} \dot{U}_{k} \\ \dot{u}_{j} \end{bmatrix} = \begin{bmatrix} a_{0} \\ o \\ a_{0} \end{bmatrix} \begin{bmatrix} \dot{U}_{k} \\ \dot{u}_{j} \\ \dot{u}_{j} \end{bmatrix} - \begin{bmatrix} o \\ a_{0} \\ o \\ \dot{u}_{j} \end{bmatrix} \begin{bmatrix} \dot{U}_{k} \\ \dot{u}_{j} \\ \dot{u}_{j} \end{bmatrix} + \frac{g}{m} \begin{bmatrix} \dot{E}_{k} \\ \dot{E}_{j} \\ \dot{E}_{t} \end{bmatrix}$ n(Ê) 二向色性 双折射 n(w, &) n(...,12) 旋光性 n(..., Rz.) (Üx = - kx + Ex (t) + q ily B2 F- 效应 N(--, B) (石级致磁光) Uy = - ky + Ey (t) - qux B2 Üx = - Wx LR) Ux + 光弹性 n(..., k) Uly = - Wilk) Uly + Kerr Box n(..., IEI) P-35/2 mü = k(u-u0)2 = ku2-zku0u+ku62 n(-, 1E) 劣粒

非线性谐振子

=> mü ≈ - zku.u